



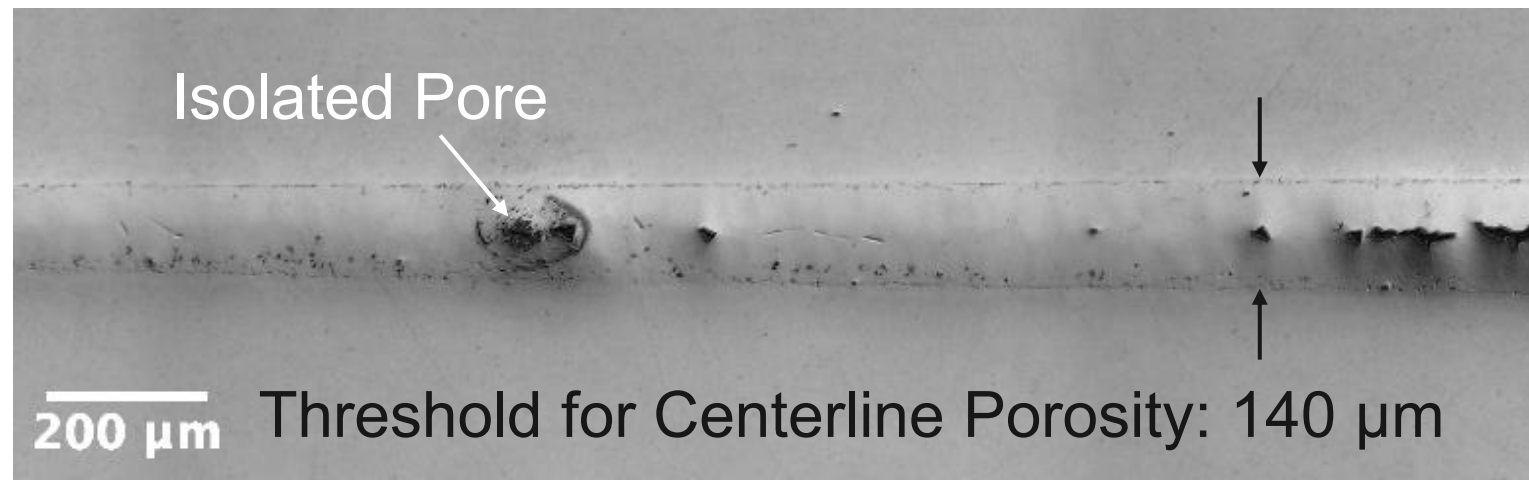
Assessment of Joint Clearance Sensitivity for a New Brazing Filler Alloy

Sammy Buk, Dr. Schneiderman, Dr. Yu | Colorado School of Mines, Golden, CO

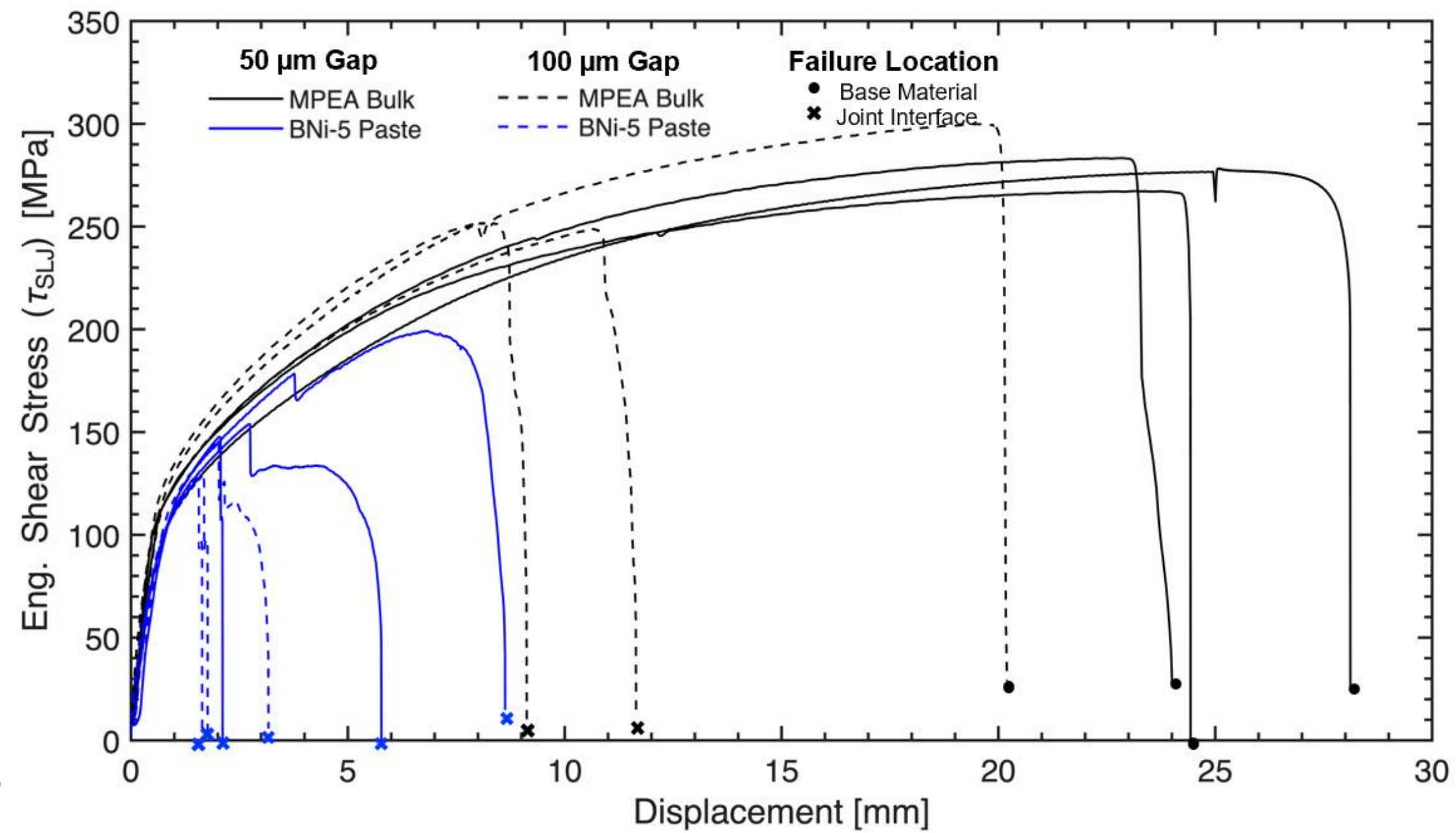


Problem Statement and Objective

- Joint clearance determines the capillary pressure driving the liquid flow into the brazing gap. It also governs mechanical strength of a brazed joint by inducing plastic constraint on the filler metal, owing to the typical higher strength of the surrounding base metal. [1]
- At fixed joint clearances of 50µm and 100µm gaps on 316L stainless steel substrate, a new multi-principal element alloy (MPEA) developed in our previous work [2] exhibited enhanced mechanical behavior in comparison to BNi-5.
- However, the MPEA filler exhibited [2] centerline defects at large gap size (e.g. centerline porosity).
- The objective of this work is to evaluate the flowability and defect formation of the new MPEA filler alloy as a function of joint clearance using a variable-gap T-joint configuration with optimal braze parameters.



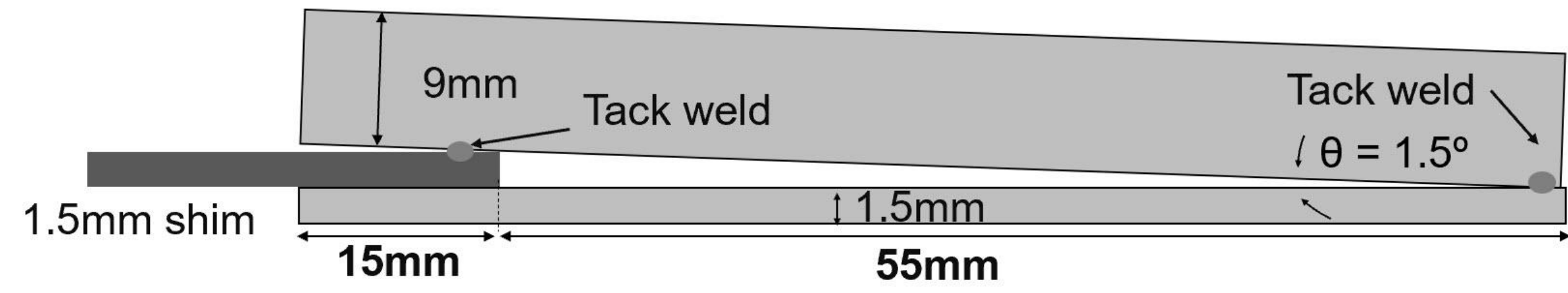
316L substrate brazed with the new MPEA filler paste applied along the joint gap parallel to length direction



Stress Strain Curve of BNi-5 vs. MPEA Shear [2]

Methodology

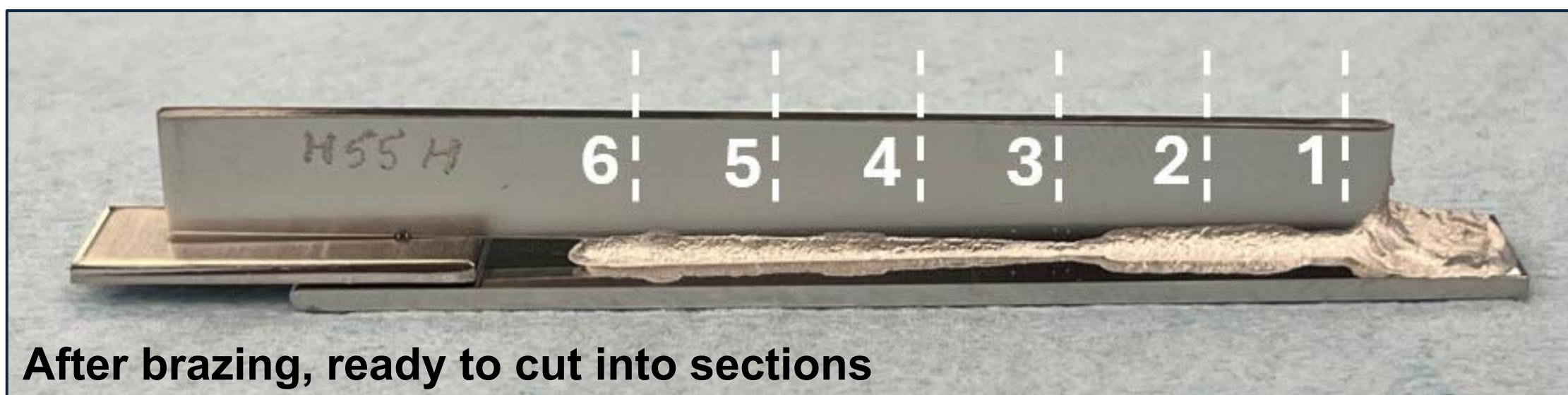
- A single T-joint specimen was designed to reveal the brazeability of the new MPEA filler as a function of clearance gap in comparison to BNi-5.
- The stem is laser tack welded onto the flange on both ends and both sides.



- Filler paste with 2x the volume of the gap was applied at the touching end to evaluate the flowability of the filler into the varying joint clearance.



- Parts were heated in a vacuum furnace to a thermal cycle of 15°C/min to 650°C, 60 min at 540°C, 15°C/min to 950°C, 30 min at 950°C, 25°C/min to 1200°C, 2 min at 1200°C.
- The brazed t-joints were cut into 3/8" sections with about 1/8" sections at the ends.



- This table explicitly contrasts the difference in parameters between this methodology designed to reduce voids in the published methodology.

	Published Parameter Set [2]	New Parameter Set
Brazing Hold Time (min)	15	2
Brazing Temp (°C)	1175	1200
Application Site	Along Length	At End
Filler Composition	Published MPEA	Optimized fabrication for contamination control

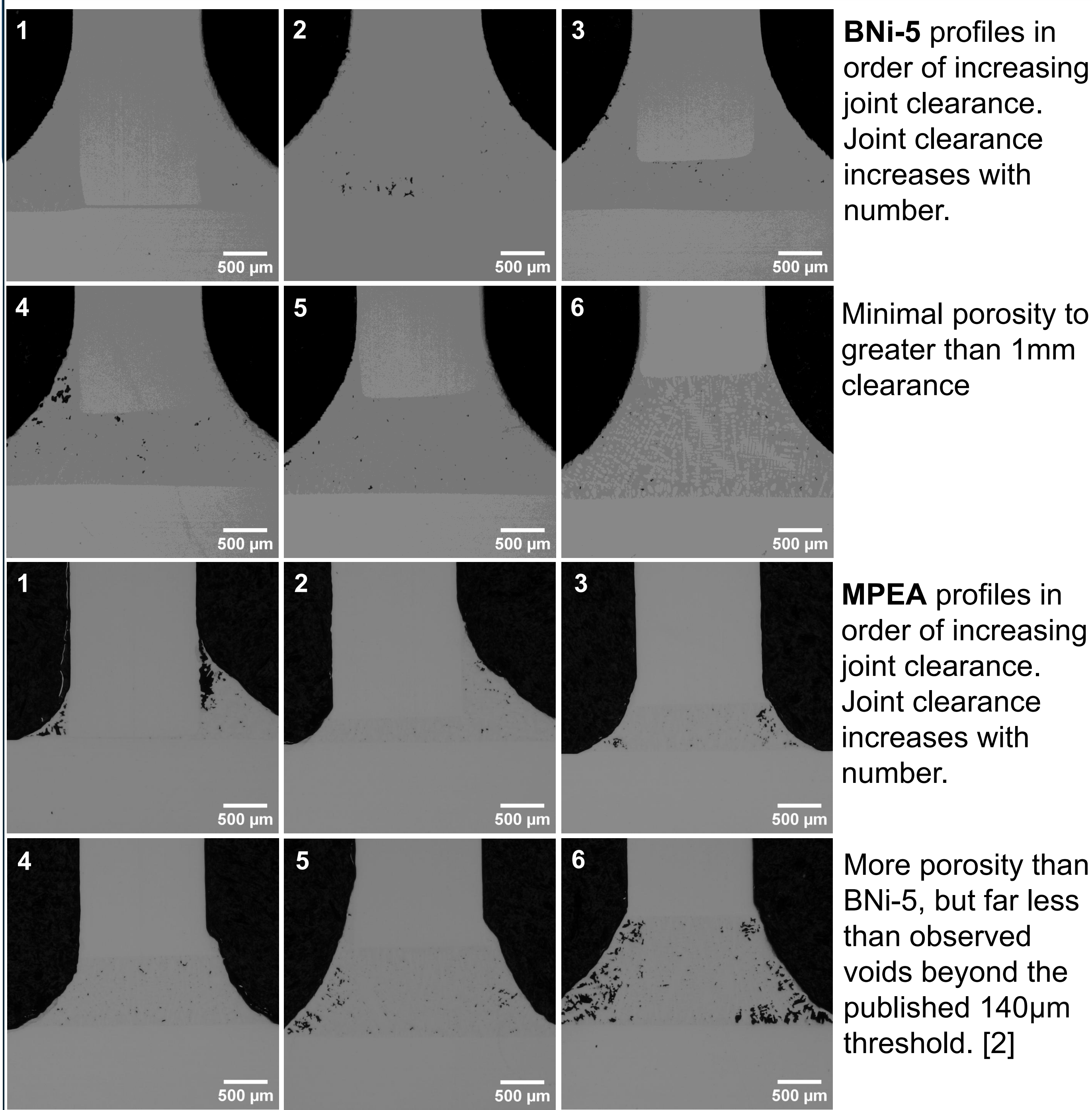
Conclusions and Future Work

- Allowing the MPEA filler to flow into the brazing joint with shorter hold time and elevated temperature resulted in less void defects in a wider clearance compared to prior published work.
- MPEA displayed strong uniform optical microstructure while the BNi-5 contained brittle secondary phases.
- Future work includes mechanical testing at gaps larger than 500µm after brazing using a new parameter set.

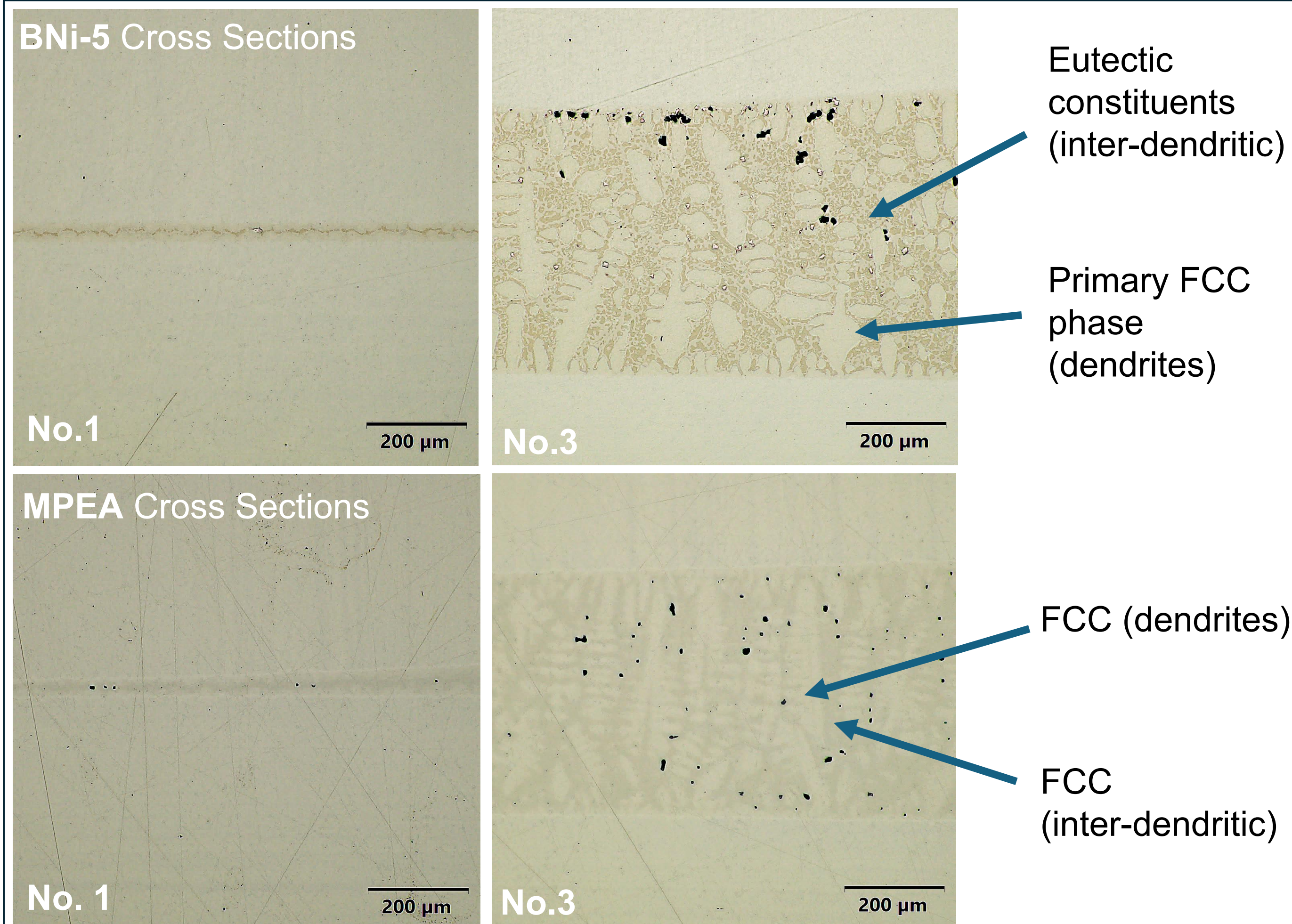
Acknowledgements

- This research is primarily supported by the National Science Foundation under SBIR Awards no. 2208777 (Phase I) and 2449209 (Phase II). We gratefully acknowledge Hoganas AB for providing BNi-5 filler paste.

Profile Results



Optical Microscopy Examination



- The mechanical degradation observed in BNi-5 shear tests is primarily driven by the brittle, Si-rich eutectic constituents (confirmed by SEM EDS, not shown here). The single-FCC microstructure (confirmed by x-ray diffraction, not shown here) of the MPEA filler significantly enhances joint mechanical performance.

References: [1] Brazing Handbook, IV ed., AWS,1991, pp. 12-25. [2] B. Schneiderman, Z. Yu et al., *Welding Journal*, 2026 (In Print).